

The Likelihood of Human Casualty in Highway Crashes

4th Briefing: Nominal Procedure & ACN Algorithms

**Based on an Investigation Conducted for
the FHWA/NHTSA Crash Analysis Center
at George Washington University, Virginia**

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"The Likelihood of Casualty in Highway Crashes"

Introduction

This is the fourth briefing concerning the cited subject. Work reported here addresses and evaluates: (a) a nominal procedure applied in the derivation of algorithms prescribed by the Automatic Collision Notification (ACN) system; (b) programmable algorithms derived by the cited procedure; and (c) illustrative results from applications of such algorithms in several cases.

Raw Data

The data compiled in the eight years, 1988-1995, of NASS/CDS are the basic data used. The NASS weights are used as weighing factors in any data processing procedure. As per suggestion of the NCSA Math Analysis Division, a "weight trimming" is applied in order to eliminate observations with a suspiciously high weight.

Specifically, observations with a weight exceeding the 98th percentile weight are excluded from consideration. Note that the processed results are not very sensitive to the introduction of "weight trimming" or to the specific value selected from trimming. Table X in this briefing compares: No Trimming, v. 2% Trimming, v. 5% Trimming for several cases.

Nominal Procedure for Processing the Raw Data

In view of the dichotomous outcome under consideration (e.g. "Yes" or "No" Fatality or MAIS 3+) a maximum likelihood procedure, specifically a logistic regression with weighing factors, is used to fit various models to the raw data. Essentially, the probability of casualty is modeled as:

$$P = 1 / [1 + \exp(-w)] \quad (1)$$

$$\text{where } w = A_0 + A_1 \cdot x_1 + A_2 \cdot x_2 + \text{etc}; \quad (2)$$

where x_1 , x_2 , etc are the selected predictors;
and A_0 , A_1 , A_2 , etc are coefficients estimated by the logistic regression.

The logistic regression also provides the covariance matrix that is needed for the estimation of variance and thus the standard error, SEP, of any predicted probability value, P.

When dealing with analyses of data from the NASS, it must be taken into account that this file contains a sample as opposed to a census of national data. In order to deal with this, the applicable statistical procedures are those prescribed in "Survey Data Analysis" (SUDAAN) software, Research Triangle Institute, Research Triangle Park, North Carolina, 1992. Such procedures are applicable in the analysis of data from multi-stage sample designs, like that of the NASS.

Estimation of Standard Errors and Confidence Bounds

The SUDAAN logistic procedure yields values for coefficients: A0, A1, A2, etc appearing in (2). The same procedure provides also the covariance matrix: COV(Ai, Aj). This helps in the calculation of the variance of the argument w of the probability appearing in (1). Specifically, the variance of w is given by:

$$\text{var}(w) = \text{Sum}[\text{Cov}(A_i, A_j) * x_i * x_j] \quad \text{over all } i \text{ and } j \quad (3)$$

Note that i or j assume the values: 0, 1, 2, etc, corresponding to the intercept and the predictors appearing in relation (2). When an analyst assigns desirable values to xi and xj, an application of (3) yields the variance: var(w).

To a first approximation the variance of the probability (1) is given by:

$$\text{var}(P) = (\exp(-2w) / [1 + \exp(-w)]^{**4}) * \text{var}(w) \quad (4)$$

and the standard error of P is:

$$\text{seP} = \text{square root} [\text{var}(P)] \quad (5)$$

Also to a first approximation, the 95% confidence bounds of P are given by: $P \pm (1.96 * \text{seP})$

Nominal Procedure Results v. Jackknife Procedure Results

As an assurance of obtaining P and seP, given by (1) and (5) of the nominal procedure, without any unexpected surprises, we compare these results with results from the simplistic jackknife procedure.

In this comparison, jackknife results are obtained from four independent and nearly equal subpopulations of the main population of raw data. Each of these four subpopulations yields a probability. A total of four: P1, P2, P3, and P4, are obtained.

These four values are used to obtain a mean and a standard error: JP and JseP, which are then compared to the: P and seP values obtained from the nominal procedure. The comparison is shown in Table VIII below for a range of predictor values.

Applications Concerning ACN Algorithms

By stipulation, all algorithms developed for this briefing concern the prediction of probability of fatality or MAIS = 2+ for car occupants in towaway crashes. Algorithms were developed for several cases of stipulated predictor availability, in order of increasing complexity, as follows:

Case I, Planar Crashes: Total Delta V, and Direction of Force;
Case I, Rollover: No or Yes.

Case II, Planar Crashes: Longitudinal and Lateral Delta V;
Case II, Rollover: No or Yes, by Number of Quarter Turns.

Case III, Planar Crashes: Total Delta V, Direction of Force,
Occupant Age and Gender, and Car Size;
Case III, Rollover: No or Yes, by Number of Quarter Turns,
Occupant Age and Gender, and Car Size;

Presentation of Programmable Algorithms

Fully detailed algorithms are presented below as follows:

| | |
|---------------------------|--------------------|
| Case I, Planar Crashes: | on Page 4 |
| Case I, Rollover: | on Page 5 |
| Case II, Planar Crashes: | on Pages 6 and 7 |
| Case II, Rollover: | on Page 8 |
| Case III, Planar Crashes: | on Pages 9 and 10 |
| Case III, Rollover: | on Pages 11 and 12 |

Results from Application of the Algorithms

Illustrative results are tabulated as follows:

| | |
|---------------------------|-----------------------|
| Case I, Planar Crashes: | Table IX on Page 14 |
| Case I, Rollover: | Table XI on Page 18 |
| Case II, Planar Crashes: | No Tabulation |
| Case II, Rollover: | Table XI on Page 18 |
| Case III, Planar Crashes: | Table XII on Page 19 |
| Case III, Rollover: | Table XIII on Page 22 |

Results are also illustrated in several figures.

Programmable Algorithm for Planar Car Crashes, Case I

Probability of Car Occupant Fatality or MAIS=2+

$$P = 1 / [1 + \exp(-w)]$$

Model:

$$w = A_0 + A_1 \cdot DVTOTAL + A_2 \cdot DOFF + A_3 \cdot DOFL + A_4 \cdot DOFR$$

DVTOTAL = Total Delta V in mph Continuously;

DOFF=1 if Direction of Force is 11 to 1 O'Clock; else DOFF=0;

DOFL=1 if Direction of Force is 8 to 10; else DOFL=0;

DOFR=1 if Direction of Force is 2 to 4; else DOFR=0;

DOFF=0 & DOFL=0 & DOFR=0 if Direction of Force is 5 to 7.

Observations used in the analysis : 20607

Number of non-zero responses: 5243

Logistic Regression Coefficients

| Predictor | A | Std Err | Probabil. of A=0 |
|-----------|-------|---------|---------------------|
| Intercept | -4.94 | 0.21 | 0.0000 |
| DVTOTAL | 0.09 | 0.00 | 0.0000 |
| DOFF | 1.34 | 0.19 | 0.0000 |
| DOFL | 1.75 | 0.20 | 0.0000 |
| DOFR | 1.70 | 0.21 | 0.0000 |

seP = square root [var(P)]

var(P) = (exp(-2w) / [1 + exp(-w)]**4) * var(w)

var(w) = Sum [Cov(Ai, Aj)*xi*xj] over all i and j

Covariance Matrix: i, j = 0 to 4

| | | | | |
|-----------|------------|-----------|-----------|-----------|
| 0.044290 | -.00039985 | -0.036158 | -0.037760 | -0.036860 |
| -0.000400 | 0.00001356 | 0.000122 | 0.000178 | 0.000141 |
| -0.036158 | 0.00012237 | 0.035375 | 0.034162 | 0.033993 |
| -0.037760 | 0.00017788 | 0.034162 | 0.041829 | 0.034549 |
| -0.036860 | 0.00014138 | 0.033993 | 0.034549 | 0.042286 |

i or j = 0 : Intercept,
 i or j = 1 : DVTOTAL,
 i or j = 2 : DOFF,
 i or j = 3 : DOFL,
 i or j = 4 : DOFR.

Programmable Algorithm for Car Rollover, Case I

Probability of Car Occupant Fatality or MAIS=2+

$$P = 1 / [1 + \exp(-w)]$$

Model:

$$w = A_0 + A_1 \cdot RO$$

RO=1 if Rollover Occurs; else RO=0

Observations used in the analysis : 51595

Number of non-zero responses: 12953

Logistic Regression Coefficients

| Predictor | A | Std Err | Probabil. of A=0 |
|-----------|-------|---------|---------------------|
| Intercept | -2.19 | 0.02 | 0.0000 |
| RO | 0.84 | 0.06 | 0.0000 |

seP = square root [var(P)]

$$\text{var}(P) = \{ \exp(-2w) / [1 + \exp(-w)]^4 \} * \text{var}(w)$$

$$\text{var}(w) = \text{Sum} [\text{Cov}(A_i, A_j) * x_i * x_j] \quad \text{over all } i \text{ and } j$$

Covariance Matrix: i, j = 0 to 1

| | |
|------------|-----------|
| 0.00043735 | -.0004400 |
| -.00043996 | 0.0037908 |

i or j = 0 : Intercept,
i or j = 1 : RO

Programmable Algorithm for Planar Car Crashes, Case II

Probability of Car Occupant Fatality or MAIS=2+

$$P = 1 / [1 + \exp(-w)]$$

Models:

$w = A_0 + A_1 \cdot DVFRONT + A_2 \cdot DVLEFT$
Observations used in the analysis : 12188
Number of non-zero responses: 3443

$w = A_0 + A_1 \cdot DVFRONT + A_2 \cdot DVRIGHT$
Observations used in the analysis : 8040
Number of non-zero responses: 2073

$w = A_0 + A_1 \cdot DVREAR + A_2 \cdot DVLEFT$
Observations used in the analysis : 2065
Number of non-zero responses: 269

$w = A_0 + A_1 \cdot DVREAR + A_2 \cdot DVRIGHT$
Observations used in the analysis : 872
Number of non-zero responses: 161

Logistic Regression Coefficients

| Predictor | A | Std Err | Probabil. of A=0 |
|-----------|-------|---------|---------------------|
| Intercept | -3.40 | 0.09 | 0.0000 |
| DVFRONT | 0.08 | 0.00 | 0.0000 |
| DVLEFT | 0.07 | 0.01 | 0.0000 |
| Intercept | -3.53 | 0.13 | 0.0000 |
| DVFRONT | 0.06 | 0.01 | 0.0000 |
| DVRIGHT | 0.09 | 0.01 | 0.0000 |
| Intercept | -3.74 | 0.32 | 0.0000 |
| DVREAR | 0.03 | 0.01 | 0.0166 |
| DVLEFT | 0.12 | 0.02 | 0.0000 |
| Intercept | -4.10 | 0.37 | 0.0000 |
| DVREAR | 0.03 | 0.01 | 0.0146 |
| DVRIGHT | 0.16 | 0.02 | 0.0000 |

Algorithm for Planar Car Crashes, Case II Cont'd

Covariance Matrices
-----Front, Left

| | | |
|-----------|------------|------------|
| 0.0089169 | -.00031967 | -.00026808 |
| -.0003197 | 0.00001757 | 0.00000268 |
| -.0002681 | 0.00000268 | 0.00003518 |

Front, Right

| | | |
|-----------|------------|------------|
| 0.015981 | -.00051074 | -.00050190 |
| -0.000511 | 0.00003126 | 0.00000150 |
| -0.000502 | 0.00000150 | 0.00004562 |

Rear, Left

| | | |
|-----------|-----------|-----------|
| 0.099364 | -.0028562 | -.0052943 |
| -0.002856 | 0.0001362 | 0.0001192 |
| -0.005294 | 0.0001192 | 0.0005231 |

Rear Right

| | | |
|----------|-----------|-----------|
| 0.14054 | -.0030133 | -.0052120 |
| -0.00301 | 0.0001858 | 0.0000424 |
| -0.00521 | 0.0000424 | 0.0003443 |

Programmable Algorithm for Car Rollover, Case II

Probability of Car Occupant Fatality or MAIS=2+

$$P = 1 / [1 + \exp(-w)]$$

Model:

$$w = A0 + A1*RO1 + A2*RO23 + A3*RO45$$

RO1=1 if Rollover Occurs with 1 Qrtr Turn; else RO1=0;
RO23=1 if Rollover Occurs with 2-3 Qrtr Turns; else RO23=0;
RO45=1 if Rollover Occurs with 4+ Qrtr Turns; else RO45=0;
If No Rollover Occurs then RO1=RO23=RO45=0.

Observations used in the analysis : 51595
Number of non-zero responses: 12953

Logistic Regression Coefficients

| Predictor | A | Std Err | Probabil. of A=0 |
|-----------|-------|---------|---------------------|
| Intercept | -2.19 | 0.02 | 0.0000 |
| RO1 | 0.40 | 0.16 | 0.0151 |
| RO23 | 0.67 | 0.09 | 0.0000 |
| RO45 | 1.15 | 0.09 | 0.0000 |

Covariance Matrix

| | | | |
|------------|-----------|-----------|-----------|
| 0.00043735 | -0.000443 | -.0004404 | -.0004384 |
| -.00044290 | 0.027118 | 0.0004399 | 0.0004422 |
| -.00044036 | 0.000440 | 0.0089888 | 0.0004390 |
| -.00043836 | 0.000442 | 0.0004390 | 0.0075658 |

Programmable Algorithm for Planar Car Crashes, Case III

Probability of Car Occupant Fatality or MAIS=2+

$$P = 1 / [1 + \exp(-w)]$$

Model:

$$w = A0 + A1*DVTOTAL + A2*DOFF + A3*DOFL + A4*DOFR + A5*AGE + A6*CARM + A7*CARM + A8*GENDER$$

DVTOTAL = Total Delta V in mph Continuously;

DOFF=1 if Direction of Force is 11 to 1 O'Clock; else DOFF=0;

DOFL=1 if Direction of Force is 8 to 10; else DOFL=0;

DOFR=1 if Direction of Force is 2 to 4; else DOFR=0;

DOFF=DOFL=DOFR=0 if Direction of Force is 5 to 7.

AGE = Occupant Age in Years Continuously;

CARM = 1 if Car is Large; else CARM=0;

CARM = 1 if Car is Midsize; else CARM=0;

CARM = CARM = 0 if Car is Small;

GENDER = 1 if Occupant is Male; else GENDER=0.

Observations used in the analysis : 20414

Number of non-zero responses: 5234

Logistic Regression Coefficients

| Predictor | A | Std Err | Probabil. of A=0 |
|-----------|-------|---------|---------------------|
| Intercept | -5.80 | 0.25 | 0.0000 |
| DVTOTAL | 0.10 | 0.00 | 0.0000 |
| DOFF | 1.42 | 0.19 | 0.0000 |
| DOFL | 1.76 | 0.21 | 0.0000 |
| DOFR | 1.68 | 0.21 | 0.0000 |
| AGE | 0.02 | 0.00 | 0.0000 |
| CARM | 0.27 | 0.11 | 0.0149 |
| CARM | 0.21 | 0.10 | 0.0436 |
| GENDER | -0.21 | 0.07 | 0.0019 |

Algorithm for Planar Car Crashes, Case III Cont'd

Covariance Matrix (9 by 9)

| | | | | |
|------------|------------|-----------|-----------|-----------|
| 0.060510 | -.00045348 | -0.037860 | -0.038195 | -0.036203 |
| -0.000453 | 0.00001452 | 0.000141 | 0.000189 | 0.000148 |
| -0.037860 | 0.00014150 | 0.036344 | 0.034936 | 0.034723 |
| -0.038195 | 0.00018933 | 0.034936 | 0.042793 | 0.035209 |
| -0.036203 | 0.00014772 | 0.034723 | 0.035209 | 0.043578 |
| -0.000166 | 0.00000102 | 0.000023 | 0.000014 | -0.000006 |
| -0.007363 | -.00003204 | -0.001064 | -0.002914 | -0.002020 |
| -0.008458 | -.00001105 | -0.000063 | -0.001065 | -0.001576 |
| -0.002673 | 0.00000166 | 0.000226 | 0.001274 | 0.000596 |
| -.00016605 | -0.007363 | -0.008458 | -.0026729 | |
| 0.00000102 | -0.000032 | -0.000011 | 0.0000017 | |
| 0.00002298 | -0.001064 | -0.000063 | 0.0002263 | |
| 0.00001439 | -0.002914 | -0.001065 | 0.0012739 | |
| -.00000610 | -0.002020 | -0.001576 | 0.0005955 | |
| 0.00000285 | 0.000037 | 0.000025 | 0.0000037 | |
| 0.00003735 | 0.012026 | 0.008327 | -.0006014 | |
| 0.00002505 | 0.008327 | 0.010507 | -.0001454 | |
| 0.00000367 | -0.000601 | -0.000145 | 0.0046873 | |

Programmable Algorithm for Car Rollover, Case III

Probability of Car Occupant Fatality or MAIS=2+

$$P = 1 / [1 + \exp(-w)]$$

Model:

$$w = A_0 + A_1 \cdot RO1 + A_2 \cdot RO23 + A_3 \cdot RO45 + A_4 \cdot CARL + A_5 \cdot CARM + A_6 \cdot AGE + A_7 \cdot GENDER$$

RO1 = 1 if Rollover Occurs with 1 Qrtr Turn; else RO1=0;
 RO23 = 1 if Rollover Occurs with 2-3 Qrtr Turns; else RO23=0;
 RO45 = 1 if Rollover Occurs with 4+ Qrtr Turns; else RO45=0;
 RO1 = RO23 = RO45 = 0 if No Rollover Occurs.
 CARL = 1 if Car is Large; else CARL=0;
 CARM = 1 if Car is Midsize; else CARM=0;
 CARL = CARM = 0 if Car is Small;
 AGE = Occupant Age in Years Continuously;
 GENDER = 1 if Occupant is Male; else GENDER=0.

Observations used in the analysis : 50924
 Number of non-zero responses: 12926

Logistic Regression Coefficients

| Predictor | A | Std Err | Probabil. of A=0 |
|-----------|-------|---------|---------------------|
| Intercept | -2.79 | 0.07 | 0.0000 |
| RO1 | 0.44 | 0.16 | 0.0075 |
| RO23 | 0.77 | 0.10 | 0.0000 |
| RO45 | 1.22 | 0.09 | 0.0000 |
| CARL | 0.22 | 0.06 | 0.0006 |
| CARM | 0.15 | 0.06 | 0.0095 |
| AGE | 0.02 | 0.00 | 0.0000 |
| GENDER | -0.09 | 0.04 | 0.0226 |

Algorithm for Car Rollover, Case III Cont'd

Covariance Matrix (8 by 8)

| | | | | |
|-----------|-------------|-----------|-----------|-----------|
| 0.0051307 | -0.000247 | -.0004844 | -.0004424 | -.0031744 |
| -.0002474 | 0.027039 | 0.0006082 | 0.0005991 | -.0005564 |
| -.0004844 | 0.000608 | 0.0091662 | 0.0006062 | -.0004122 |
| -.0004424 | 0.000599 | 0.0006062 | 0.0078184 | -.0004039 |
| -.0031744 | -0.000556 | -.0004122 | -.0004039 | 0.0039996 |
| -.0030607 | -0.000281 | -.0000712 | -.0001950 | 0.0028011 |
| -.0000458 | 0.000006 | 0.0000085 | 0.0000072 | 0.0000115 |
| -.0009395 | -0.000200 | -.0001890 | -.0000374 | 0.0000291 |
| | | | | |
| -.0030607 | -.000045804 | -.0009395 | | |
| -.0002812 | 0.000006332 | -.0001996 | | |
| -.0000712 | 0.000008528 | -.0001890 | | |
| -.0001950 | 0.000007176 | -.0000374 | | |
| 0.0028011 | 0.000011550 | 0.0000291 | | |
| 0.0035527 | 0.000006859 | 0.0001640 | | |
| 0.0000069 | 0.000001075 | 0.0000015 | | |
| 0.0001640 | 0.000001549 | 0.0015871 | | |

Table VIII.

Probability of Fatality or MAIS=3+ for 30 Yr Old Drivers in Frontal Crashes; Comparison of Results from Nominal Procedure with Jackknife Results.

P, SEP = Probability & Std Error from Nominal Procedure;

P1 to P4 = Probabilities from Four Jackknifed Subpopulations;

JP, JSEP = Mean and Std Error of P1 to P4.

| Restrained | | | | | | | | |
|------------|------|------|------|------|------|------|-------|------|
| DV | P | SEP | P1 | P2 | P3 | P4 | JP | JSEP |
| 5 | 0.3 | 0.04 | 0.3 | 0.2 | 0.4 | 0.2 | 0.28 | 0.05 |
| 10 | 0.5 | 0.07 | 0.6 | 0.3 | 0.7 | 0.4 | 0.50 | 0.09 |
| 15 | 0.9 | 0.11 | 1.0 | 0.6 | 1.2 | 0.7 | 0.88 | 0.14 |
| 20 | 1.6 | 0.18 | 1.9 | 1.3 | 2.2 | 1.4 | 1.70 | 0.21 |
| 25 | 2.8 | 0.30 | 3.4 | 2.6 | 3.9 | 2.6 | 3.13 | 0.32 |
| 30 | 5.0 | 0.52 | 6.0 | 5.0 | 6.8 | 4.9 | 5.68 | 0.45 |
| 35 | 8.8 | 0.91 | 10.3 | 9.6 | 11.8 | 9.0 | 10.18 | 0.60 |
| 40 | 14.9 | 1.56 | 17.4 | 17.7 | 19.6 | 16.0 | 17.68 | 0.74 |
| 45 | 24.2 | 2.49 | 27.7 | 30.2 | 30.8 | 26.7 | 28.85 | 0.98 |
| 50 | 36.8 | 3.51 | 41.1 | 46.5 | 44.8 | 41.1 | 43.38 | 1.36 |
| 55 | 51.5 | 4.19 | 56.0 | 63.6 | 59.6 | 57.2 | 59.10 | 1.68 |
| 60 | 65.9 | 4.18 | 69.8 | 77.9 | 72.9 | 71.9 | 73.13 | 1.72 |
| 65 | 77.9 | 3.54 | 80.8 | 87.7 | 83.1 | 83.1 | 83.68 | 1.45 |
| 70 | 86.5 | 2.63 | 88.5 | 93.5 | 89.9 | 90.4 | 90.58 | 1.05 |
| 75 | 92.1 | 1.79 | 93.3 | 96.6 | 94.2 | 94.7 | 94.70 | 0.70 |
| 80 | 95.5 | 1.15 | 96.2 | 98.3 | 96.7 | 97.2 | 97.10 | 0.45 |
| 85 | 97.5 | 0.71 | 97.9 | 99.2 | 98.2 | 98.5 | 98.45 | 0.28 |
| 90 | 98.6 | 0.43 | 98.8 | 99.6 | 99.0 | 99.2 | 99.15 | 0.17 |

| Unrestrained | | | | | | | | |
|--------------|------|------|------|------|------|------|-------|------|
| DV | P | SEP | P1 | P2 | P3 | P4 | JP | JSEP |
| 5 | 0.7 | 0.11 | 0.4 | 0.6 | 1.1 | 0.6 | 0.68 | 0.15 |
| 10 | 1.2 | 0.18 | 0.7 | 1.2 | 1.9 | 1.1 | 1.23 | 0.25 |
| 15 | 2.2 | 0.30 | 1.3 | 2.4 | 3.4 | 2.2 | 2.33 | 0.43 |
| 20 | 3.9 | 0.48 | 2.4 | 4.7 | 6.1 | 4.1 | 4.33 | 0.77 |
| 25 | 6.9 | 0.79 | 4.3 | 8.9 | 10.5 | 7.5 | 7.80 | 1.32 |
| 30 | 11.9 | 1.27 | 7.5 | 16.5 | 17.7 | 13.5 | 13.80 | 2.28 |
| 35 | 19.8 | 1.96 | 12.9 | 28.5 | 28.1 | 23.0 | 23.13 | 3.63 |
| 40 | 31.0 | 2.79 | 21.2 | 44.5 | 41.6 | 36.4 | 35.93 | 5.19 |
| 45 | 45.0 | 3.49 | 33.0 | 61.8 | 56.5 | 52.2 | 50.88 | 6.27 |
| 50 | 59.9 | 3.72 | 47.3 | 76.5 | 70.3 | 67.7 | 65.45 | 6.33 |
| 55 | 73.1 | 3.35 | 62.0 | 86.8 | 81.2 | 80.1 | 77.53 | 5.38 |
| 60 | 83.2 | 2.62 | 74.8 | 93.0 | 88.7 | 88.5 | 86.25 | 3.96 |
| 65 | 90.0 | 1.85 | 84.4 | 96.4 | 93.5 | 93.6 | 91.98 | 2.61 |
| 70 | 94.3 | 1.22 | 90.8 | 98.2 | 96.3 | 96.6 | 95.48 | 1.61 |
| 75 | 96.8 | 0.77 | 94.7 | 99.1 | 97.9 | 98.2 | 97.48 | 0.96 |
| 80 | 98.2 | 0.47 | 97.0 | 99.5 | 98.9 | 99.0 | 98.60 | 0.55 |
| 85 | 99.0 | 0.28 | 98.4 | 99.8 | 99.4 | 99.5 | 99.28 | 0.30 |
| 90 | 99.5 | 0.17 | 99.1 | 99.9 | 99.7 | 99.7 | 99.60 | 0.17 |

Table IX.

Results from Application of Algorithm for Case I,
Planar Car Crashes: Probability of Fatality or MAIS=2+.

| Direction of Force | DeltaV | Probab. & Std Err | | 95% Confid. Bounds | |
|-----------------------|--------|-------------------|-----|--------------------|-------|
| | | P | seP | Lower | Upper |
| 11-1 | 5 | 4.1 | 0.3 | 3.5 | 4.7 |
| 11-1 | 10 | 6.3 | 0.3 | 5.7 | 6.9 |
| 11-1 | 15 | 9.5 | 0.4 | 8.7 | 10.3 |
| 11-1 | 20 | 14.2 | 0.5 | 13.2 | 15.2 |
| 11-1 | 25 | 20.6 | 0.7 | 19.2 | 22.0 |
| 11-1 | 30 | 28.9 | 1.1 | 26.7 | 31.1 |
| 11-1 | 35 | 38.9 | 1.6 | 35.8 | 42.0 |
| 11-1 | 40 | 50.0 | 2.1 | 45.9 | 54.1 |
| 11-1 | 45 | 61.1 | 2.4 | 56.4 | 65.8 |
| 11-1 | 50 | 71.1 | 2.4 | 66.4 | 75.8 |
| 11-1 | 55 | 79.4 | 2.2 | 75.1 | 83.7 |
| 11-1 | 60 | 85.8 | 1.8 | 82.3 | 89.3 |
| 11-1 | 65 | 90.5 | 1.5 | 87.6 | 93.4 |
| 11-1 | 70 | 93.7 | 1.1 | 91.5 | 95.9 |
| 11-1 | 75 | 95.9 | 0.8 | 94.3 | 97.5 |
| 11-1 | 80 | 97.3 | 0.6 | 96.1 | 98.5 |
| 11-1 | 85 | 98.3 | 0.4 | 97.5 | 99.1 |
| 11-1 | 90 | 98.9 | 0.3 | 98.3 | 99.5 |
| 2-4 | 5 | 5.8 | 0.6 | 4.6 | 7.0 |
| 2-4 | 10 | 8.8 | 0.8 | 7.2 | 10.4 |
| 2-4 | 15 | 13.1 | 1.0 | 11.1 | 15.1 |
| 2-4 | 20 | 19.2 | 1.4 | 16.5 | 21.9 |
| 2-4 | 25 | 27.1 | 1.8 | 23.6 | 30.6 |
| 2-4 | 30 | 36.8 | 2.3 | 32.3 | 41.3 |
| 2-4 | 35 | 47.8 | 2.7 | 42.5 | 53.1 |
| 2-4 | 40 | 58.9 | 2.9 | 53.2 | 64.6 |
| 2-4 | 45 | 69.2 | 2.8 | 63.7 | 74.7 |
| 2-4 | 50 | 77.9 | 2.5 | 73.0 | 82.8 |
| 2-4 | 55 | 84.7 | 2.1 | 80.6 | 88.8 |
| 2-4 | 60 | 89.7 | 1.6 | 86.6 | 92.8 |
| 2-4 | 65 | 93.2 | 1.2 | 90.8 | 95.6 |
| 2-4 | 70 | 95.5 | 0.9 | 93.7 | 97.3 |
| 2-4 | 75 | 97.1 | 0.6 | 95.9 | 98.3 |
| 2-4 | 80 | 98.1 | 0.4 | 97.3 | 98.9 |
| 2-4 | 85 | 98.8 | 0.3 | 98.2 | 99.4 |
| 2-4 | 90 | 99.2 | 0.2 | 98.8 | 99.6 |
| 8-10 | 5 | 6.1 | 0.5 | 5.1 | 7.1 |
| 8-10 | 10 | 9.2 | 0.7 | 7.8 | 10.6 |
| 8-10 | 15 | 13.7 | 1.0 | 11.7 | 15.7 |

Table IX. Cont'd

| | | | | | |
|------|----|------|-----|------|------|
| 8-10 | 20 | 19.9 | 1.3 | 17.4 | 22.4 |
| 8-10 | 25 | 28.1 | 1.8 | 24.6 | 31.6 |
| 8-10 | 30 | 38.0 | 2.3 | 33.5 | 42.5 |
| 8-10 | 35 | 49.0 | 2.7 | 43.7 | 54.3 |
| 8-10 | 40 | 60.1 | 2.9 | 54.4 | 65.8 |
| 8-10 | 45 | 70.3 | 2.8 | 64.8 | 75.8 |
| 8-10 | 50 | 78.8 | 2.5 | 73.9 | 83.7 |
| 8-10 | 55 | 85.3 | 2.1 | 81.2 | 89.4 |
| 8-10 | 60 | 90.1 | 1.6 | 87.0 | 93.2 |
| 8-10 | 65 | 93.5 | 1.2 | 91.1 | 95.9 |
| 8-10 | 70 | 95.7 | 0.9 | 93.9 | 97.5 |
| 8-10 | 75 | 97.2 | 0.6 | 96.0 | 98.4 |
| 8-10 | 80 | 98.2 | 0.4 | 97.4 | 99.0 |
| 8-10 | 85 | 98.9 | 0.3 | 98.3 | 99.5 |
| 8-10 | 90 | 99.3 | 0.2 | 98.9 | 99.7 |
| 5-7 | 5 | 1.1 | 0.2 | 0.7 | 1.5 |
| 5-7 | 10 | 1.7 | 0.3 | 1.1 | 2.3 |
| 5-7 | 15 | 2.7 | 0.5 | 1.7 | 3.7 |
| 5-7 | 20 | 4.1 | 0.7 | 2.7 | 5.5 |
| 5-7 | 25 | 6.4 | 1.1 | 4.2 | 8.6 |
| 5-7 | 30 | 9.6 | 1.6 | 6.5 | 12.7 |
| 5-7 | 35 | 14.3 | 2.2 | 10.0 | 18.6 |
| 5-7 | 40 | 20.8 | 3.0 | 14.9 | 26.7 |
| 5-7 | 45 | 29.1 | 3.9 | 21.5 | 36.7 |
| 5-7 | 50 | 39.2 | 4.7 | 30.0 | 48.4 |
| 5-7 | 55 | 50.2 | 5.1 | 40.2 | 60.2 |
| 5-7 | 60 | 61.3 | 5.0 | 51.5 | 71.1 |
| 5-7 | 65 | 71.3 | 4.6 | 62.3 | 80.3 |
| 5-7 | 70 | 79.6 | 3.8 | 72.2 | 87.0 |
| 5-7 | 75 | 85.9 | 3.0 | 80.0 | 91.8 |
| 5-7 | 80 | 90.6 | 2.2 | 86.3 | 94.9 |
| 5-7 | 85 | 93.8 | 1.6 | 90.7 | 96.9 |
| 5-7 | 90 | 95.9 | 1.1 | 93.7 | 98.1 |

Table X.

Effect of NASS Weight Trimming on the Results Given in
Table IX (Nominal Procedure).

| DOF | DELTA V | Nominal Procedure | | | | | |
|------|---------|-------------------|-----|-------------|-----|-------------|-----|
| | | No Trimming | | 2% Trimming | | 5% Trimming | |
| | | P | SEP | P | SEP | P | SEP |
| 11-1 | 5 | 2.9 | 0.2 | 4.1 | 0.3 | 4.5 | 0.3 |
| 11-1 | 10 | 4.7 | 0.3 | 6.3 | 0.3 | 6.8 | 0.3 |
| 11-1 | 15 | 7.4 | 0.4 | 9.5 | 0.4 | 10.3 | 0.4 |
| 11-1 | 20 | 11.7 | 0.5 | 14.2 | 0.5 | 15.3 | 0.5 |
| 11-1 | 25 | 17.9 | 0.8 | 20.6 | 0.7 | 22.1 | 0.7 |
| 11-1 | 30 | 26.5 | 1.3 | 28.9 | 1.1 | 30.8 | 1.1 |
| 11-1 | 35 | 37.3 | 2.0 | 38.9 | 1.6 | 41.1 | 1.5 |
| 11-1 | 40 | 49.5 | 2.6 | 50.0 | 2.1 | 52.2 | 1.9 |
| 11-1 | 45 | 61.8 | 2.9 | 61.1 | 2.4 | 63.2 | 2.2 |
| 11-1 | 50 | 72.7 | 2.8 | 71.1 | 2.4 | 72.9 | 2.2 |
| 11-1 | 55 | 81.5 | 2.4 | 79.4 | 2.2 | 80.8 | 2.0 |
| 11-1 | 60 | 87.9 | 1.9 | 85.8 | 1.8 | 86.9 | 1.6 |
| 11-1 | 65 | 92.3 | 1.4 | 90.5 | 1.5 | 91.2 | 1.3 |
| 11-1 | 70 | 95.2 | 1.0 | 93.7 | 1.1 | 94.2 | 1.0 |
| 11-1 | 75 | 97.0 | 0.7 | 95.9 | 0.8 | 96.2 | 0.7 |
| 11-1 | 80 | 98.2 | 0.5 | 97.3 | 0.6 | 97.6 | 0.5 |
| 11-1 | 85 | 98.9 | 0.3 | 98.3 | 0.4 | 98.4 | 0.4 |
| 11-1 | 90 | 99.3 | 0.2 | 98.9 | 0.3 | 99.0 | 0.2 |
| 2-4 | 5 | 4.4 | 0.5 | 5.8 | 0.6 | 6.2 | 0.5 |
| 2-4 | 10 | 7.0 | 0.8 | 8.8 | 0.8 | 9.4 | 0.7 |
| 2-4 | 15 | 11.1 | 1.1 | 13.1 | 1.0 | 14.1 | 1.0 |
| 2-4 | 20 | 17.1 | 1.6 | 19.2 | 1.4 | 20.4 | 1.3 |
| 2-4 | 25 | 25.4 | 2.3 | 27.1 | 1.8 | 28.7 | 1.7 |
| 2-4 | 30 | 35.9 | 2.9 | 36.8 | 2.3 | 38.7 | 2.1 |
| 2-4 | 35 | 48.0 | 3.4 | 47.8 | 2.7 | 49.8 | 2.5 |
| 2-4 | 40 | 60.3 | 3.6 | 58.9 | 2.9 | 60.8 | 2.7 |
| 2-4 | 45 | 71.5 | 3.3 | 69.2 | 2.8 | 70.9 | 2.6 |
| 2-4 | 50 | 80.5 | 2.8 | 77.9 | 2.5 | 79.2 | 2.3 |
| 2-4 | 55 | 87.2 | 2.2 | 84.7 | 2.1 | 85.7 | 1.9 |
| 2-4 | 60 | 91.8 | 1.6 | 89.7 | 1.6 | 90.4 | 1.5 |
| 2-4 | 65 | 94.9 | 1.1 | 93.2 | 1.2 | 93.6 | 1.1 |
| 2-4 | 70 | 96.8 | 0.8 | 95.5 | 0.9 | 95.9 | 0.8 |
| 2-4 | 75 | 98.1 | 0.5 | 97.1 | 0.6 | 97.3 | 0.6 |
| 2-4 | 80 | 98.8 | 0.3 | 98.1 | 0.4 | 98.3 | 0.4 |
| 2-4 | 85 | 99.3 | 0.2 | 98.8 | 0.3 | 98.9 | 0.3 |
| 2-4 | 90 | 99.6 | 0.1 | 99.2 | 0.2 | 99.3 | 0.2 |
| 8-10 | 5 | 4.1 | 0.4 | 6.1 | 0.5 | 6.2 | 0.5 |
| 8-10 | 10 | 6.5 | 0.6 | 9.2 | 0.7 | 9.4 | 0.6 |

Table X. Cont'd

| | | | | | | | |
|------|----|------|-----|------|-----|------|-----|
| 8-10 | 15 | 10.3 | 0.8 | 13.7 | 1.0 | 13.9 | 0.9 |
| 8-10 | 20 | 16.0 | 1.2 | 19.9 | 1.3 | 20.3 | 1.2 |
| 8-10 | 25 | 23.9 | 1.8 | 28.1 | 1.8 | 28.5 | 1.6 |
| 8-10 | 30 | 34.1 | 2.4 | 38.0 | 2.3 | 38.5 | 2.0 |
| 8-10 | 35 | 46.0 | 3.0 | 49.0 | 2.7 | 49.5 | 2.4 |
| 8-10 | 40 | 58.4 | 3.3 | 60.1 | 2.9 | 60.6 | 2.6 |
| 8-10 | 45 | 69.8 | 3.2 | 70.3 | 2.8 | 70.7 | 2.6 |
| 8-10 | 50 | 79.2 | 2.8 | 78.8 | 2.5 | 79.1 | 2.3 |
| 8-10 | 55 | 86.3 | 2.2 | 85.3 | 2.1 | 85.6 | 1.9 |
| 8-10 | 60 | 91.2 | 1.6 | 90.1 | 1.6 | 90.3 | 1.5 |
| 8-10 | 65 | 94.5 | 1.2 | 93.5 | 1.2 | 93.6 | 1.1 |
| 8-10 | 70 | 96.6 | 0.8 | 95.7 | 0.9 | 95.8 | 0.8 |
| 8-10 | 75 | 97.9 | 0.5 | 97.2 | 0.6 | 97.3 | 0.6 |
| 8-10 | 80 | 98.7 | 0.4 | 98.2 | 0.4 | 98.3 | 0.4 |
| 8-10 | 85 | 99.2 | 0.2 | 98.9 | 0.3 | 98.9 | 0.3 |
| 8-10 | 90 | 99.5 | 0.2 | 99.3 | 0.2 | 99.3 | 0.2 |
| 5-7 | 5 | 0.6 | 0.1 | 1.1 | 0.2 | 1.1 | 0.2 |
| 5-7 | 10 | 1.0 | 0.2 | 1.7 | 0.3 | 1.8 | 0.3 |
| 5-7 | 15 | 1.6 | 0.4 | 2.7 | 0.5 | 2.7 | 0.4 |
| 5-7 | 20 | 2.6 | 0.6 | 4.1 | 0.7 | 4.2 | 0.7 |
| 5-7 | 25 | 4.3 | 0.9 | 6.4 | 1.1 | 6.5 | 1.0 |
| 5-7 | 30 | 6.8 | 1.4 | 9.6 | 1.6 | 9.8 | 1.5 |
| 5-7 | 35 | 10.8 | 2.1 | 14.3 | 2.2 | 14.6 | 2.1 |
| 5-7 | 40 | 16.7 | 3.1 | 20.8 | 3.0 | 21.1 | 2.9 |
| 5-7 | 45 | 24.8 | 4.2 | 29.1 | 3.9 | 29.5 | 3.7 |
| 5-7 | 50 | 35.2 | 5.3 | 39.2 | 4.7 | 39.7 | 4.5 |
| 5-7 | 55 | 47.3 | 6.0 | 50.2 | 5.1 | 50.7 | 4.9 |
| 5-7 | 60 | 59.6 | 6.1 | 61.3 | 5.0 | 61.8 | 4.9 |
| 5-7 | 65 | 70.9 | 5.5 | 71.3 | 4.6 | 71.7 | 4.4 |
| 5-7 | 70 | 80.1 | 4.4 | 79.6 | 3.8 | 79.9 | 3.7 |
| 5-7 | 75 | 86.9 | 3.3 | 85.9 | 3.0 | 86.2 | 2.9 |
| 5-7 | 80 | 91.6 | 2.3 | 90.6 | 2.2 | 90.7 | 2.1 |
| 5-7 | 85 | 94.7 | 1.6 | 93.8 | 1.6 | 93.9 | 1.5 |
| 5-7 | 90 | 96.7 | 1.1 | 95.9 | 1.1 | 96.0 | 1.1 |

Table XI.

Results from Application of Algorithm for Cases I & II,
Car Rollover: Probability of Fatality or MAIS=2+.

| Case I Rollover | Qrtr Turns | Probab. & Std Err | | 95% Confid. Bounds | |
|--------------------|---------------|-------------------|-----|--------------------|-------|
| | | P | seP | Lower | Upper |
| No | 0 | 10.1 | 0.2 | 9.7 | 10.5 |
| Yes | Any | 20.6 | 0.9 | 18.8 | 22.4 |

Case II

| | | | | | |
|-----|-----|------|-----|------|------|
| No | 0 | 10.1 | 0.2 | 9.7 | 10.5 |
| Yes | 1 | 14.3 | 2.0 | 10.4 | 18.2 |
| Yes | 2-3 | 17.9 | 1.4 | 15.2 | 20.6 |
| Yes | 4+ | 26.1 | 1.6 | 23.0 | 29.2 |

Table XII.

Selected Results from Application of Algorithm for
Case III, Planar Car Crashes.

Probability P of Fatality or MAIS=2+, and Std Error seP

| Item | Total DeltaV | Force Directn | Occpnt Age | Occpnt Gender | Car Size | P | seP |
|------|-----------------|------------------|---------------|------------------|-------------|------|-----|
| 1 | 10 | 8-10 | 15 | Male | Large | 5.0 | 0.7 |
| 2 | 10 | 8-10 | 15 | Male | Small | 6.4 | 0.7 |
| 3 | 10 | 8-10 | 15 | Female | Large | 6.1 | 0.8 |
| 4 | 10 | 8-10 | 15 | Female | Small | 7.8 | 0.8 |
| 5 | 10 | 8-10 | 75 | Male | Large | 14.8 | 1.8 |
| 6 | 10 | 8-10 | 75 | Male | Small | 18.5 | 1.9 |
| 7 | 10 | 8-10 | 75 | Female | Large | 17.7 | 1.9 |
| 8 | 10 | 8-10 | 75 | Female | Small | 21.9 | 2.0 |
| 9 | 10 | 5-7 | 15 | Male | Large | 0.9 | 0.2 |
| 10 | 10 | 5-7 | 15 | Male | Small | 1.2 | 0.2 |
| 11 | 10 | 5-7 | 15 | Female | Large | 1.1 | 0.2 |
| 12 | 10 | 5-7 | 15 | Female | Small | 1.4 | 0.3 |
| 13 | 10 | 5-7 | 75 | Male | Large | 2.9 | 0.6 |
| 14 | 10 | 5-7 | 75 | Male | Small | 3.8 | 0.8 |
| 15 | 10 | 5-7 | 75 | Female | Large | 3.6 | 0.7 |
| 16 | 10 | 5-7 | 75 | Female | Small | 4.6 | 1.0 |
| 17 | 20 | 8-10 | 15 | Male | Large | 12.5 | 1.6 |
| 18 | 20 | 8-10 | 15 | Male | Small | 15.7 | 1.4 |
| 19 | 20 | 8-10 | 15 | Female | Large | 14.9 | 1.7 |
| 20 | 20 | 8-10 | 15 | Female | Small | 18.7 | 1.5 |
| 21 | 20 | 8-10 | 75 | Male | Large | 32.1 | 3.2 |
| 22 | 20 | 8-10 | 75 | Male | Small | 38.2 | 2.9 |
| 23 | 20 | 8-10 | 75 | Female | Large | 36.8 | 3.2 |
| 24 | 20 | 8-10 | 75 | Female | Small | 43.3 | 2.9 |
| 25 | 20 | 5-7 | 15 | Male | Large | 2.4 | 0.5 |
| 26 | 20 | 5-7 | 15 | Male | Small | 3.1 | 0.6 |
| 27 | 20 | 5-7 | 15 | Female | Large | 2.9 | 0.6 |
| 28 | 20 | 5-7 | 15 | Female | Small | 3.8 | 0.7 |
| 29 | 20 | 5-7 | 75 | Male | Large | 7.5 | 1.4 |
| 30 | 20 | 5-7 | 75 | Male | Small | 9.6 | 1.8 |
| 31 | 20 | 5-7 | 75 | Female | Large | 9.1 | 1.7 |
| 32 | 20 | 5-7 | 75 | Female | Small | 11.6 | 2.2 |
| 33 | 30 | 8-10 | 15 | Male | Large | 27.9 | 3.1 |
| 34 | 30 | 8-10 | 15 | Male | Small | 33.8 | 2.5 |
| 35 | 30 | 8-10 | 15 | Female | Large | 32.3 | 3.2 |
| 36 | 30 | 8-10 | 15 | Female | Small | 38.5 | 2.6 |
| 37 | 30 | 8-10 | 75 | Male | Large | 56.2 | 3.9 |
| 38 | 30 | 8-10 | 75 | Male | Small | 62.7 | 3.2 |
| 39 | 30 | 8-10 | 75 | Female | Large | 61.3 | 3.5 |

Table XII. Cont'd

| | | | | | | | |
|----|----|------|----|--------|-------|------|-----|
| 40 | 30 | 8-10 | 75 | Female | Small | 67.5 | 2.9 |
| 41 | 30 | 5-7 | 15 | Male | Large | 6.2 | 1.2 |
| 42 | 30 | 5-7 | 15 | Male | Small | 8.0 | 1.4 |
| 43 | 30 | 5-7 | 15 | Female | Large | 7.6 | 1.5 |
| 44 | 30 | 5-7 | 15 | Female | Small | 9.7 | 1.7 |
| 45 | 30 | 5-7 | 75 | Male | Large | 18.1 | 3.0 |
| 46 | 30 | 5-7 | 75 | Male | Small | 22.4 | 3.6 |
| 47 | 30 | 5-7 | 75 | Female | Large | 21.4 | 3.5 |
| 48 | 30 | 5-7 | 75 | Female | Small | 26.3 | 4.0 |
| 49 | 40 | 8-10 | 15 | Male | Large | 51.2 | 4.2 |
| 50 | 40 | 8-10 | 15 | Male | Small | 57.9 | 3.2 |
| 51 | 40 | 8-10 | 15 | Female | Large | 56.5 | 4.0 |
| 52 | 40 | 8-10 | 15 | Female | Small | 62.9 | 3.0 |
| 53 | 40 | 8-10 | 75 | Male | Large | 77.7 | 3.0 |
| 54 | 40 | 8-10 | 75 | Male | Small | 82.1 | 2.3 |
| 55 | 40 | 8-10 | 75 | Female | Large | 81.2 | 2.6 |
| 56 | 40 | 8-10 | 75 | Female | Small | 84.9 | 1.9 |
| 57 | 40 | 5-7 | 15 | Male | Large | 15.3 | 2.7 |
| 58 | 40 | 5-7 | 15 | Male | Small | 19.2 | 3.0 |
| 59 | 40 | 5-7 | 15 | Female | Large | 18.2 | 3.1 |
| 60 | 40 | 5-7 | 15 | Female | Small | 22.6 | 3.5 |
| 61 | 40 | 5-7 | 75 | Male | Large | 37.5 | 5.0 |
| 62 | 40 | 5-7 | 75 | Male | Small | 44.0 | 5.2 |
| 63 | 40 | 5-7 | 75 | Female | Large | 42.6 | 5.2 |
| 64 | 40 | 5-7 | 75 | Female | Small | 49.3 | 5.3 |
| 65 | 50 | 8-10 | 15 | Male | Large | 74.1 | 3.7 |
| 66 | 50 | 8-10 | 15 | Male | Small | 78.9 | 2.6 |
| 67 | 50 | 8-10 | 15 | Female | Large | 77.9 | 3.2 |
| 68 | 50 | 8-10 | 15 | Female | Small | 82.2 | 2.3 |
| 69 | 50 | 8-10 | 75 | Male | Large | 90.5 | 1.7 |
| 70 | 50 | 8-10 | 75 | Male | Small | 92.6 | 1.3 |
| 71 | 50 | 8-10 | 75 | Female | Large | 92.1 | 1.4 |
| 72 | 50 | 8-10 | 75 | Female | Small | 93.9 | 1.0 |
| 73 | 50 | 5-7 | 15 | Male | Large | 33.0 | 4.9 |
| 74 | 50 | 5-7 | 15 | Male | Small | 39.2 | 4.9 |
| 75 | 50 | 5-7 | 15 | Female | Large | 37.8 | 5.2 |
| 76 | 50 | 5-7 | 15 | Female | Small | 44.3 | 5.2 |
| 77 | 50 | 5-7 | 75 | Male | Large | 62.0 | 5.3 |
| 78 | 50 | 5-7 | 75 | Male | Small | 68.1 | 4.8 |
| 79 | 50 | 5-7 | 75 | Female | Large | 66.8 | 5.0 |
| 80 | 50 | 5-7 | 75 | Female | Small | 72.5 | 4.5 |
| 81 | 60 | 8-10 | 15 | Male | Large | 88.6 | 2.2 |
| 82 | 60 | 8-10 | 15 | Male | Small | 91.1 | 1.5 |
| 83 | 60 | 8-10 | 15 | Female | Large | 90.6 | 1.8 |
| 84 | 60 | 8-10 | 15 | Female | Small | 92.6 | 1.3 |
| 85 | 60 | 8-10 | 75 | Male | Large | 96.3 | 0.8 |
| 86 | 60 | 8-10 | 75 | Male | Small | 97.1 | 0.6 |
| 87 | 60 | 8-10 | 75 | Female | Large | 97.0 | 0.7 |

Table XII. Concluded

| | | | | | | | |
|----|----|------|----|--------|-------|------|-----|
| 88 | 60 | 8-10 | 75 | Female | Small | 97.7 | 0.5 |
| 89 | 60 | 5-7 | 15 | Male | Large | 57.2 | 5.8 |
| 90 | 60 | 5-7 | 15 | Male | Small | 63.6 | 5.1 |
| 91 | 60 | 5-7 | 15 | Female | Large | 62.2 | 5.6 |
| 92 | 60 | 5-7 | 15 | Female | Small | 68.4 | 4.9 |
| 93 | 60 | 5-7 | 75 | Male | Large | 81.6 | 3.6 |
| 94 | 60 | 5-7 | 75 | Male | Small | 85.3 | 3.0 |
| 95 | 60 | 5-7 | 75 | Female | Large | 84.6 | 3.2 |
| 96 | 60 | 5-7 | 75 | Female | Small | 87.8 | 2.6 |

Table XIII.

Results from Application of Algorithm for Case III,
Car Rollover: Probability of Fatality or MAIS=2+.

Rollover with 4+ Quarter Turns

| OCCAGE | GENDER | CAR | P | SEP |
|--------|--------|-------|------|-----|
| 15 | Male | Large | 20.4 | 1.7 |
| 15 | Male | Mid | 23.0 | 1.6 |
| 15 | Male | Small | 24.2 | 1.6 |
| 15 | Female | Large | 21.9 | 1.8 |
| 15 | Female | Mid | 24.6 | 1.7 |
| 15 | Female | Small | 25.9 | 1.8 |
| 30 | Male | Large | 25.7 | 2.0 |
| 30 | Male | Mid | 28.7 | 1.9 |
| 30 | Male | Small | 30.2 | 1.9 |
| 30 | Female | Large | 27.5 | 2.1 |
| 30 | Female | Mid | 30.6 | 1.9 |
| 30 | Female | Small | 32.1 | 2.0 |
| 45 | Male | Large | 31.9 | 2.2 |
| 45 | Male | Mid | 35.2 | 2.1 |
| 45 | Male | Small | 36.8 | 2.1 |
| 45 | Female | Large | 33.8 | 2.3 |
| 45 | Female | Mid | 37.3 | 2.1 |
| 45 | Female | Small | 38.9 | 2.2 |
| 60 | Male | Large | 38.7 | 2.5 |
| 60 | Male | Mid | 42.3 | 2.4 |
| 60 | Male | Small | 44.0 | 2.4 |
| 60 | Female | Large | 40.9 | 2.6 |
| 60 | Female | Mid | 44.5 | 2.4 |
| 60 | Female | Small | 46.3 | 2.4 |
| 75 | Male | Large | 46.0 | 2.7 |
| 75 | Male | Mid | 49.8 | 2.6 |
| 75 | Male | Small | 51.5 | 2.6 |
| 75 | Female | Large | 48.3 | 2.8 |
| 75 | Female | Mid | 52.0 | 2.5 |
| 75 | Female | Small | 53.7 | 2.6 |

Rollover with 2-3 Quarter Turns

| OCCAGE | GENDER | CAR | P | SEP |
|--------|--------|-------|------|-----|
| 15 | Male | Large | 14.1 | 1.3 |
| 15 | Male | Mid | 16.0 | 1.3 |
| 15 | Male | Small | 16.9 | 1.3 |
| 15 | Female | Large | 15.2 | 1.4 |

Table XIII. Cont'd

| | | | | |
|----|--------|-------|------|-----|
| 15 | Female | Mid | 17.2 | 1.4 |
| 15 | Female | Small | 18.2 | 1.5 |
| 30 | Male | Large | 18.1 | 1.6 |
| 30 | Male | Mid | 20.4 | 1.6 |
| 30 | Male | Small | 21.6 | 1.6 |
| 30 | Female | Large | 19.5 | 1.7 |
| 30 | Female | Mid | 21.9 | 1.7 |
| 30 | Female | Small | 23.1 | 1.7 |
| 45 | Male | Large | 23.0 | 1.9 |
| 45 | Male | Mid | 25.7 | 1.9 |
| 45 | Male | Small | 27.1 | 1.9 |
| 45 | Female | Large | 24.6 | 2.0 |
| 45 | Female | Mid | 27.5 | 2.0 |
| 45 | Female | Small | 28.9 | 2.1 |
| 60 | Male | Large | 28.7 | 2.3 |
| 60 | Male | Mid | 31.9 | 2.2 |
| 60 | Male | Small | 33.4 | 2.3 |
| 60 | Female | Large | 30.6 | 2.4 |
| 60 | Female | Mid | 33.8 | 2.3 |
| 60 | Female | Small | 35.4 | 2.4 |
| 75 | Male | Large | 35.2 | 2.6 |
| 75 | Male | Mid | 38.7 | 2.6 |
| 75 | Male | Small | 40.4 | 2.6 |
| 75 | Female | Large | 37.3 | 2.7 |
| 75 | Female | Mid | 40.9 | 2.7 |
| 75 | Female | Small | 42.6 | 2.7 |

Rollover with 1 Quarter Turn

| OCCAGE | GENDER | CAR | P | SEP |
|--------|--------|-------|------|-----|
| 15 | Male | Large | 10.5 | 1.6 |
| 15 | Male | Mid | 12.0 | 1.8 |
| 15 | Male | Small | 12.8 | 1.8 |
| 15 | Female | Large | 11.4 | 1.8 |
| 15 | Female | Mid | 13.0 | 1.9 |
| 15 | Female | Small | 13.8 | 2.0 |
| 30 | Male | Large | 13.7 | 2.0 |
| 30 | Male | Mid | 15.6 | 2.2 |
| 30 | Male | Small | 16.5 | 2.3 |
| 30 | Female | Large | 14.8 | 2.2 |
| 30 | Female | Mid | 16.8 | 2.3 |
| 30 | Female | Small | 17.8 | 2.4 |
| 45 | Male | Large | 17.7 | 2.5 |
| 45 | Male | Mid | 19.9 | 2.7 |
| 45 | Male | Small | 21.1 | 2.8 |
| 45 | Female | Large | 19.0 | 2.7 |
| 45 | Female | Mid | 21.4 | 2.8 |

Table XIII. Cont'd

| | | | | |
|----|--------|-------|------|-----|
| 45 | Female | Small | 22.6 | 2.9 |
| 60 | Male | Large | 22.4 | 3.0 |
| 60 | Male | Mid | 25.2 | 3.2 |
| 60 | Male | Small | 26.5 | 3.3 |
| 60 | Female | Large | 24.0 | 3.2 |
| 60 | Female | Mid | 26.9 | 3.3 |
| 60 | Female | Small | 28.3 | 3.4 |
| 75 | Male | Large | 28.1 | 3.6 |
| 75 | Male | Mid | 31.2 | 3.7 |
| 75 | Male | Small | 32.7 | 3.8 |
| 75 | Female | Large | 29.9 | 3.7 |
| 75 | Female | Mid | 33.2 | 3.8 |
| 75 | Female | Small | 34.8 | 3.9 |

No Rollover

| OCCAGE | GENDER | CAR | P | SEP |
|--------|--------|-------|------|-----|
| 15 | Male | Large | . | . |
| 15 | Male | Mid | . | . |
| 15 | Male | Small | 8.6 | 0.3 |
| 15 | Female | Large | . | . |
| 15 | Female | Mid | . | . |
| 15 | Female | Small | 9.4 | 0.4 |
| 30 | Male | Large | 9.3 | 0.5 |
| 30 | Male | Mid | 10.6 | 0.3 |
| 30 | Male | Small | 11.3 | 0.4 |
| 30 | Female | Large | 10.1 | 0.5 |
| 30 | Female | Mid | 11.5 | 0.4 |
| 30 | Female | Small | 12.2 | 0.4 |
| 45 | Male | Large | 12.1 | 0.6 |
| 45 | Male | Mid | 13.8 | 0.4 |
| 45 | Male | Small | 14.7 | 0.5 |
| 45 | Female | Large | 13.1 | 0.6 |
| 45 | Female | Mid | 14.9 | 0.4 |
| 45 | Female | Small | 15.8 | 0.6 |
| 60 | Male | Large | 15.7 | 0.8 |
| 60 | Male | Mid | 17.8 | 0.7 |
| 60 | Male | Small | 18.8 | 0.8 |
| 60 | Female | Large | 16.9 | 0.8 |
| 60 | Female | Mid | 19.2 | 0.6 |
| 60 | Female | Small | 20.3 | 0.8 |
| 75 | Male | Large | 20.1 | 1.0 |
| 75 | Male | Mid | 22.6 | 1.0 |
| 75 | Male | Small | 23.9 | 1.1 |
| 75 | Female | Large | 21.6 | 1.1 |
| 75 | Female | Mid | 24.2 | 1.0 |
| 75 | Female | Small | 25.5 | 1.2 |

Fig. 37. 95% Confidence Bounds of Probability of Fatality or MAIS 2+, in Towaway Car Crashes: An Overview

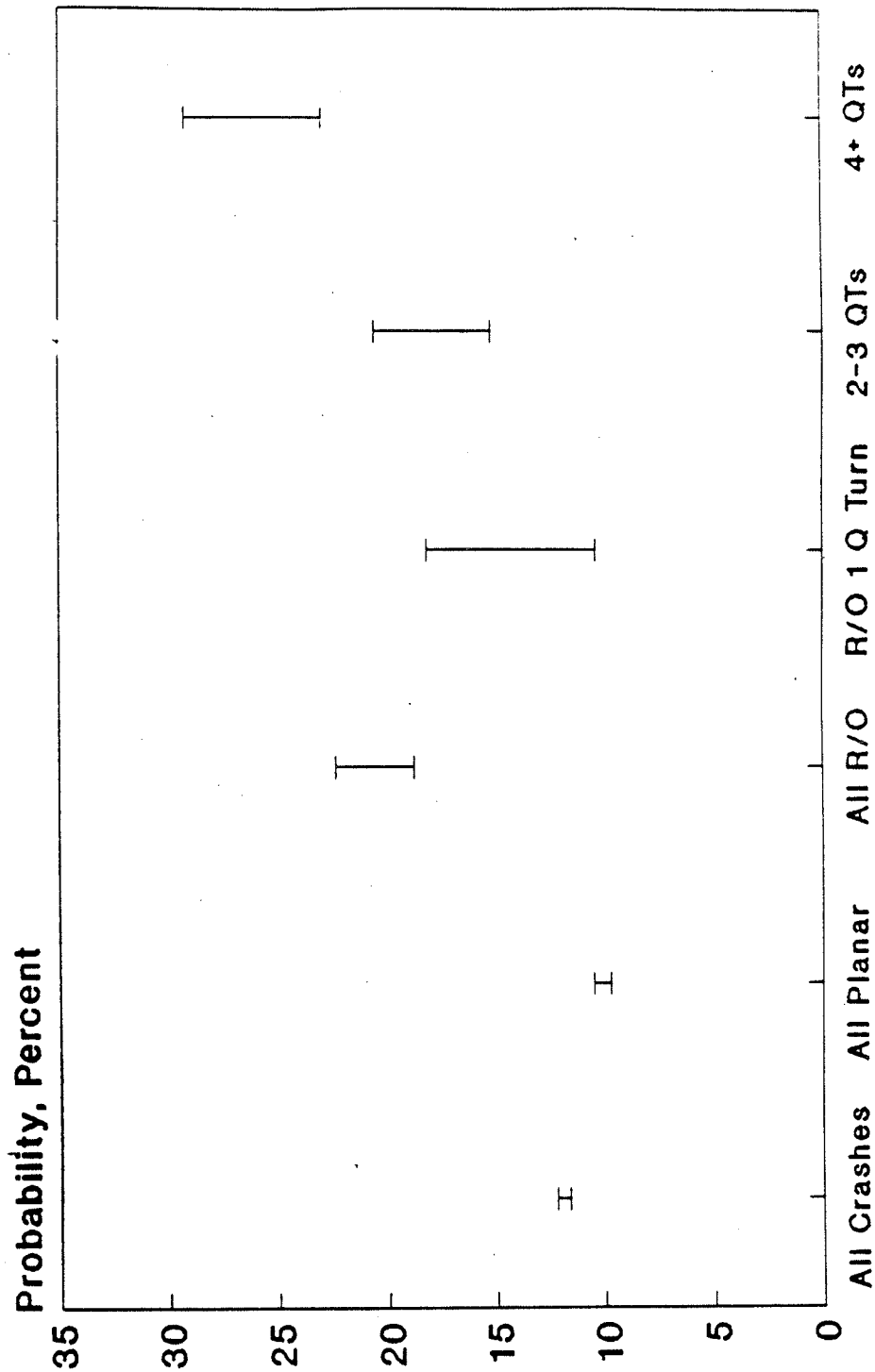


Fig. 38. Variation of Probability of Fatality or MAIS 2+, v. Delta V, for All Planar Car Crashes

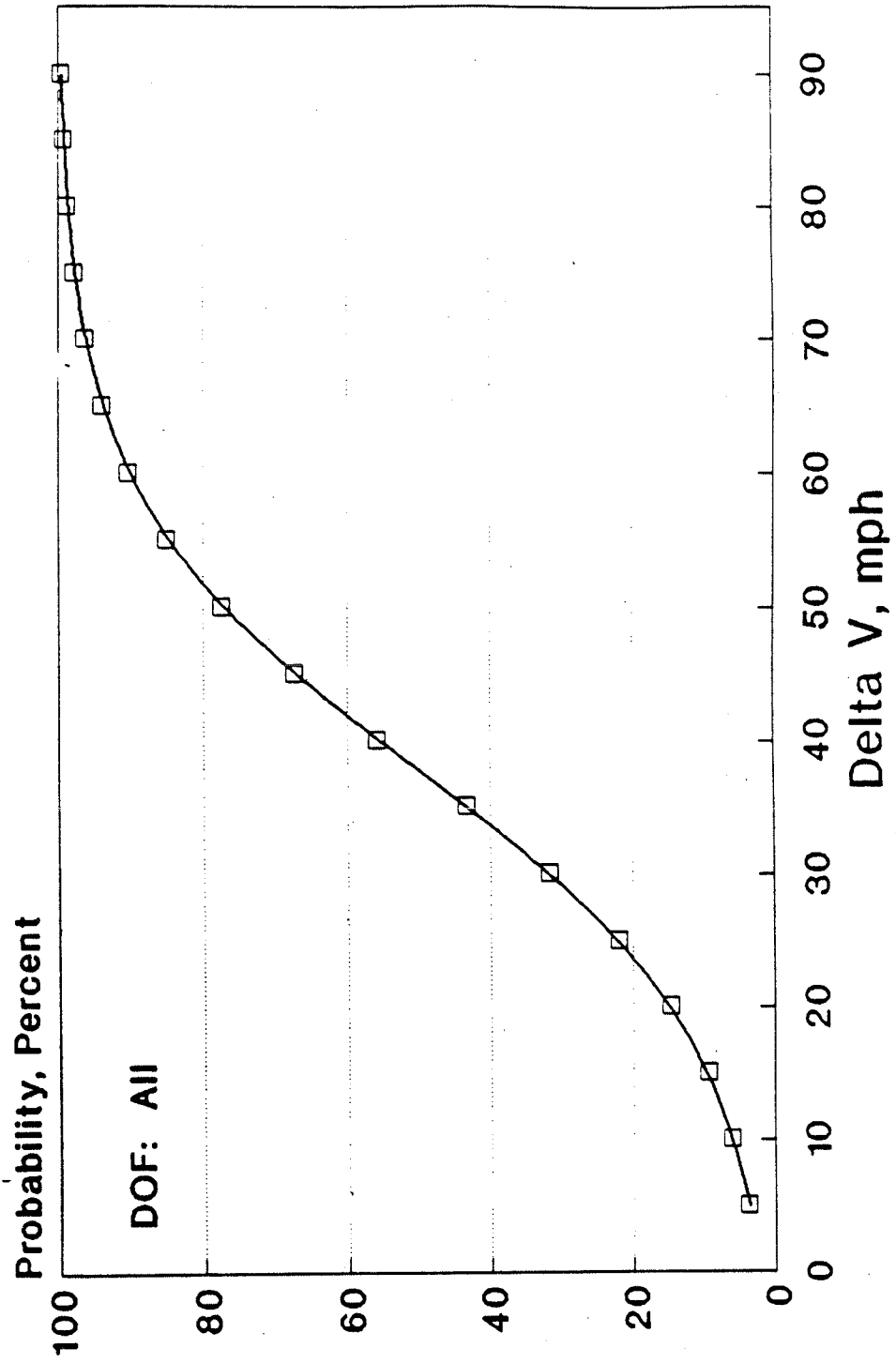


Fig. 39. 95% Confidence Bounds for
 Probability of Fatality or MAIS 2+,
 v. Delta V, in Frontal Towaway Crashes

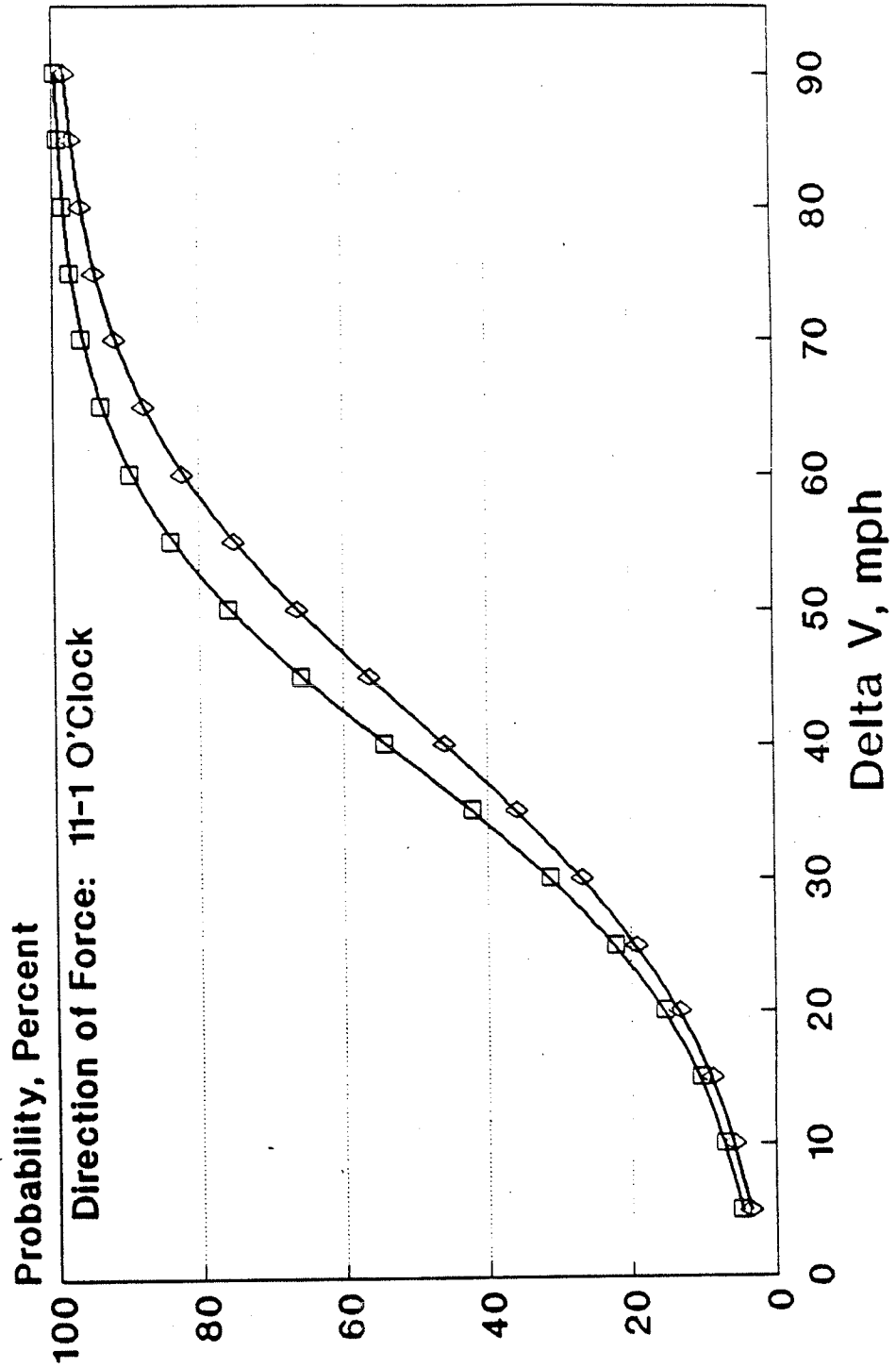


Fig. 40. 95% Confidence Bounds for
Probability of Fatality or MAIS 2+,
v. Delta V for Left Planar Car Cras

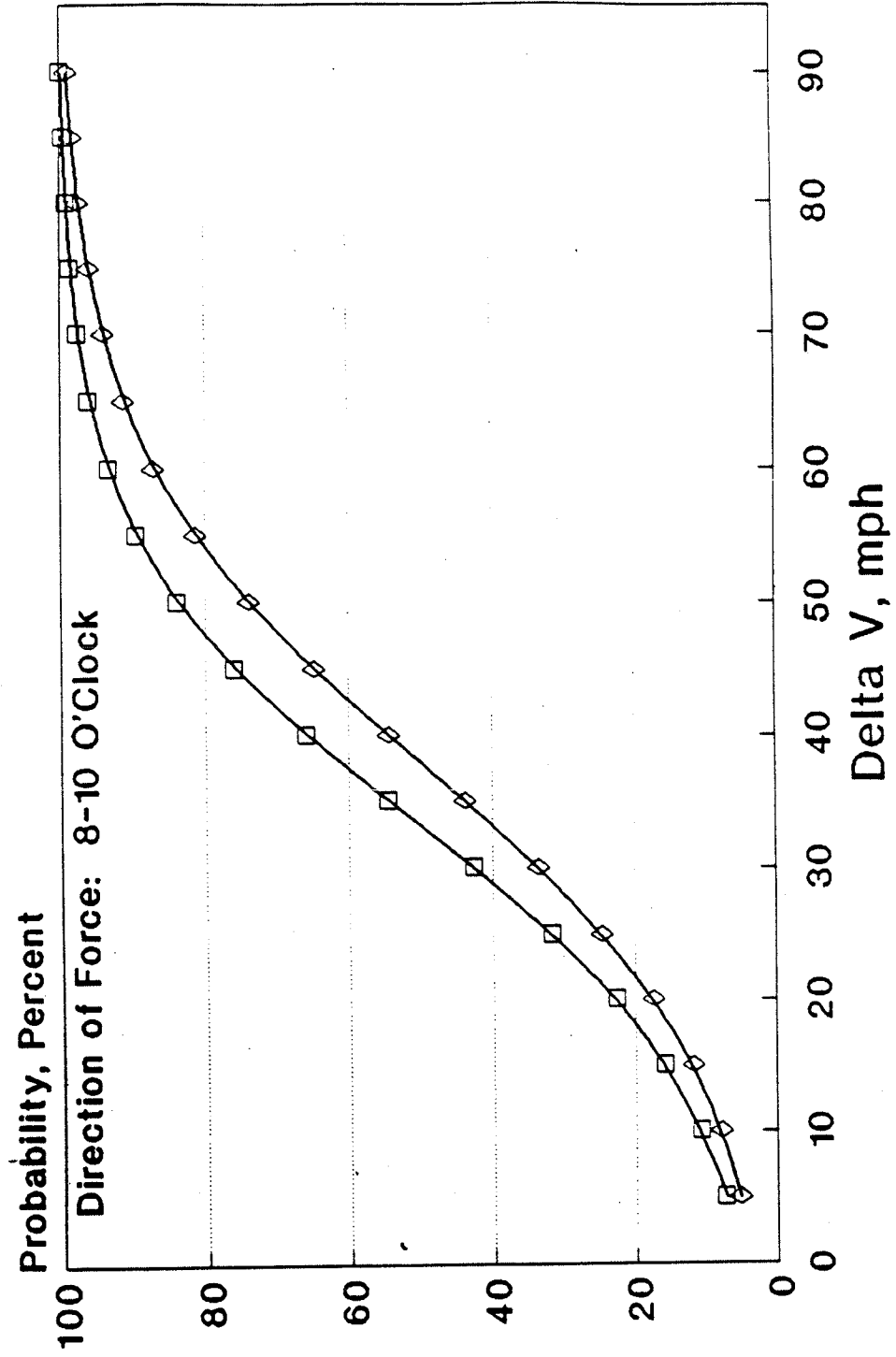


Fig. 41. 95% Confidence Bounds for
Probability of Fatality or MAIS 2+,
v. Delta V for Rear Planar Car Crashes

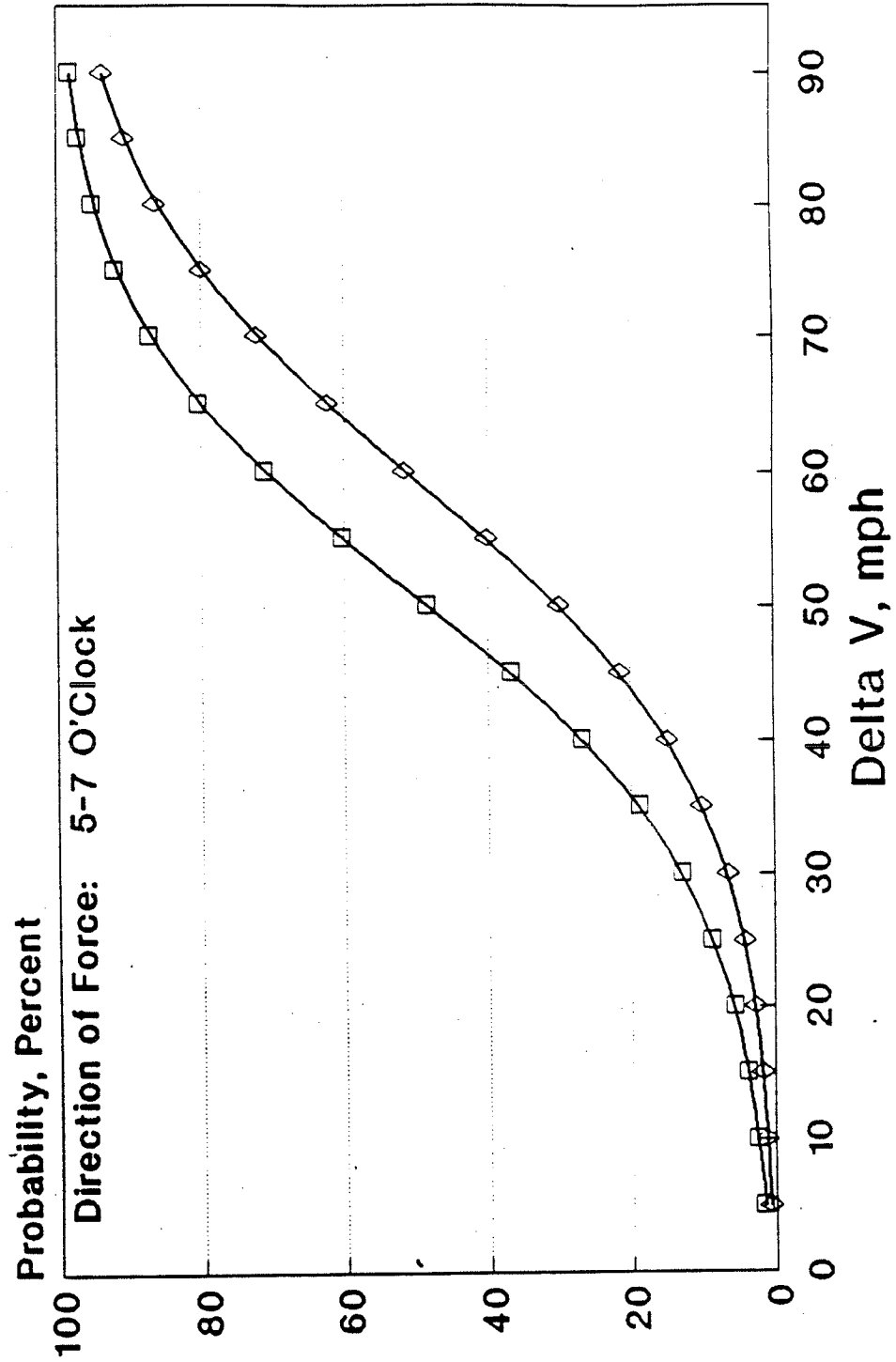


Fig. 42. 95% Confidence Bounds for
 Probability of Fatality or MAIS 2+,
 v. Delta V in Crashes of Shown Direction

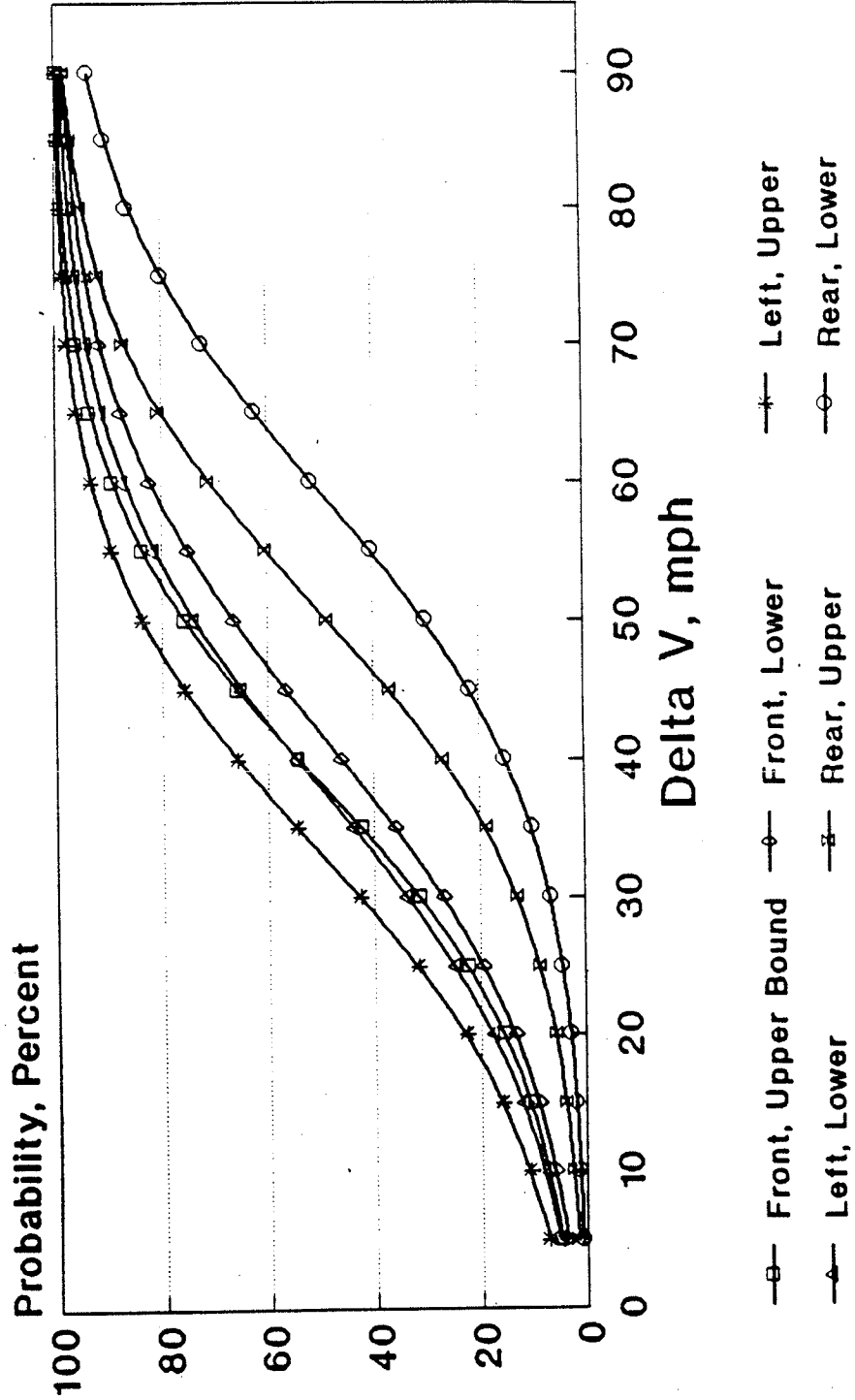


Fig. 43. 95% Confidence Bounds of Probability of Fatality or MAIS 2+, in Shown Towaway Car Crashes

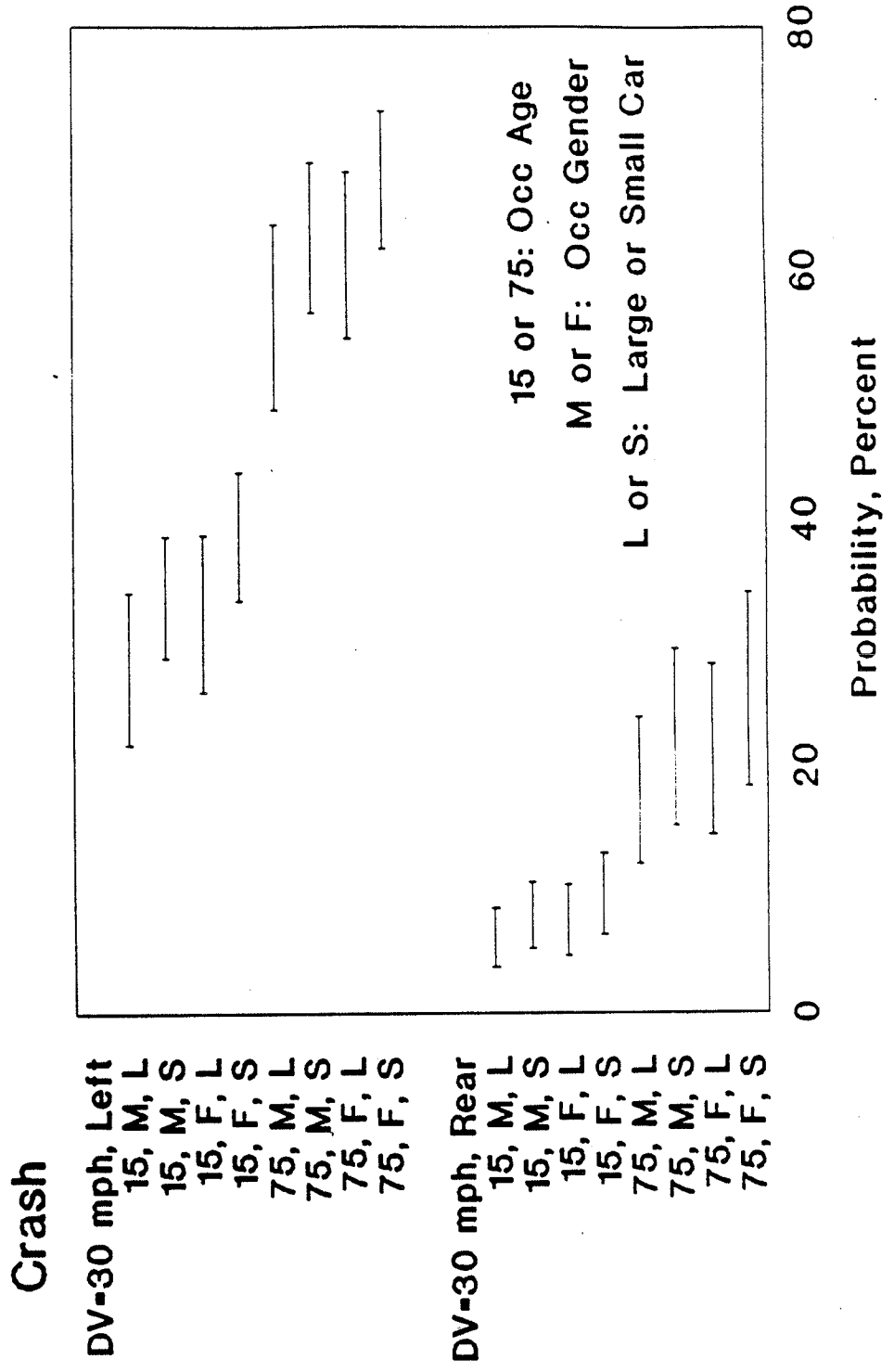


Fig. 44. 95% Confidence Bounds of Probability of Fatality or MAIS 2+; an Illustration of Extremes

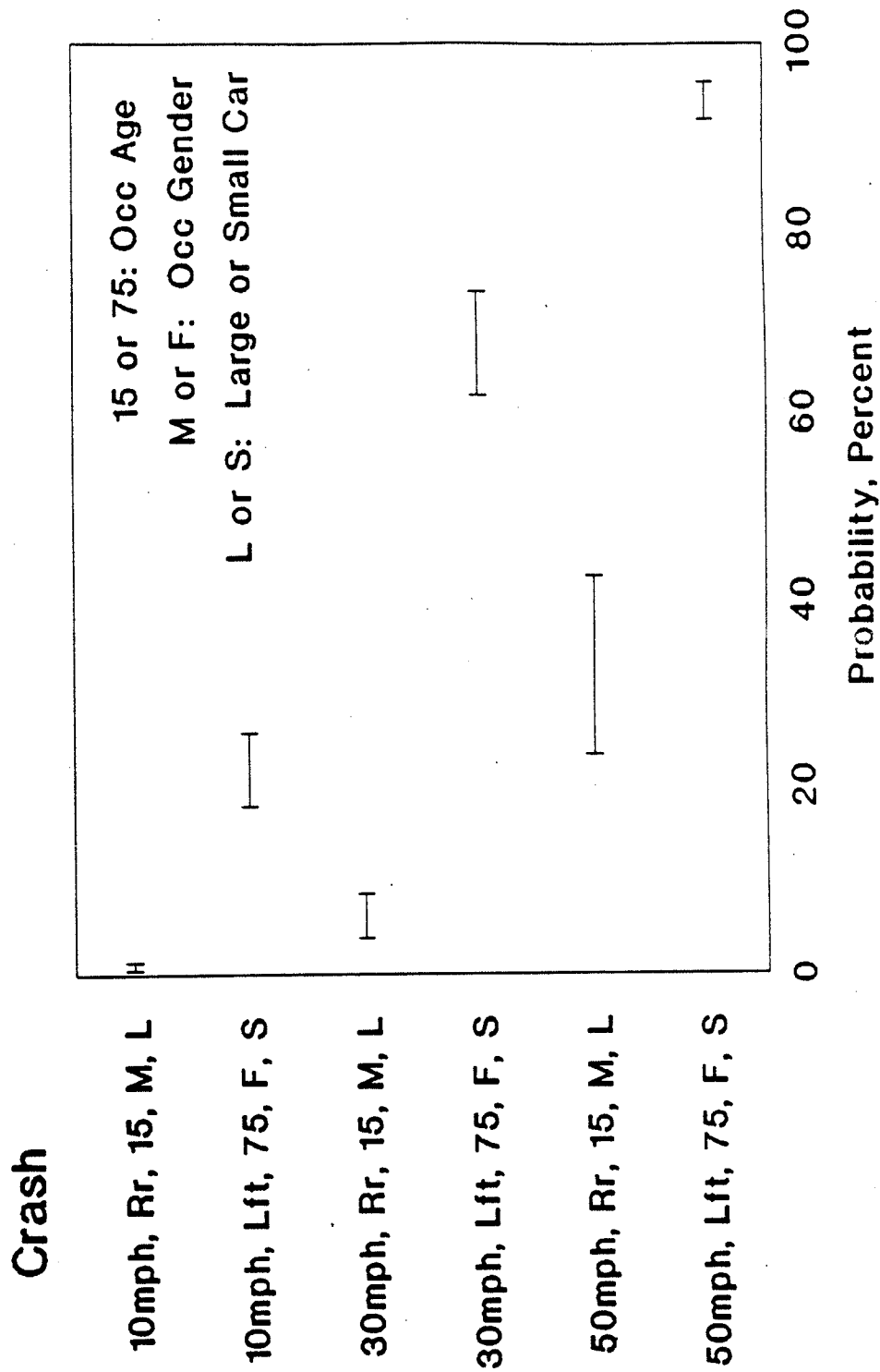


Fig. 45. 95% Confidence Bounds of Probability of Fatality or MAIS 2+, in Shown Towaway Car Rollovers

